

## A SECOND ORDER EXTENSION OF THE GENERALIZED- $\alpha$ METHOD FOR CONSTRAINED SYSTEMS IN MECHANICS

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**Abstract.** *We present a new second order extension of the generalized- $\alpha$  method for systems in mechanics with a nonconstant mass matrix, holonomic constraints, and nonholonomic constraints. A new variable stepsizes formula preserving the second order of the method is also proposed.*

## 1 INTRODUCTION

We consider second order systems of differential equations of the form  $My'' = f(t, y, y')$ . In mechanics  $M \in \mathbb{R}^{n \times n}$  is a constant mass matrix,  $y \in \mathbb{R}^n$  is a vector of generalized coordinates,  $y' \in \mathbb{R}^n$  is a vector of generalized velocities, and  $y'' \in \mathbb{R}^n$  is a vector of generalized accelerations. Introducing the new variables  $z := y' \in \mathbb{R}^n$  and  $a := z' = y'' \in \mathbb{R}^n$ , these equations are equivalent to the semi-explicit system of differential-algebraic equations (DAEs)

$$y' = z, \quad z' = a, \quad 0 = Ma - f(t, y, z). \quad (1)$$

Assuming the mass matrix  $M$  to be invertible, the system of DAEs given by Eq. (1) is of index 1 since one can obtain explicitly the relation  $a = M^{-1}f(t, y, z)$ . The generalized- $\alpha$  method of Chung and Hulbert (see Ref. [2]) for  $My'' = f(t, y, y')$  or equivalently for Eq. (1) is a non-standard implicit one-step method. One step of the method  $(t_0, y_0, z_0, a_\alpha) \mapsto (t_1 = t_0 + h, y_1, z_1, a_{1+\alpha})$  with stepsize  $h$  can be expressed as follows

$$y_1 = y_0 + h z_0 + \frac{h^2}{2} ((1 - 2\beta)a_\alpha + 2\beta a_{1+\alpha}), \quad (2)$$

$$z_1 = z_0 + h((1 - \gamma)a_\alpha + \gamma a_{1+\alpha}), \quad (3)$$

$$(1 - \alpha_m)M a_{1+\alpha} + \alpha_m M a_\alpha = (1 - \alpha_f)f(t_1, y_1, z_1) + \alpha_f f(t_0, y_0, z_0), \quad (4)$$

see section 2 below for a justification of the notation  $a_\alpha, a_{1+\alpha}$ . The generalized- $\alpha$  method has coefficients  $\beta, \gamma, \alpha_m \neq 1, \alpha_f$ . For certain specific choices of these coefficients we obtain well-known methods:

- Newmark's family:  $\alpha_m = 0, \alpha_f = 0$ ;
  - Trapezoidal rule:  $\beta = \frac{1}{4}, \gamma = \frac{1}{2}$ ;
  - Störmer's rule:  $\beta = 0, \gamma = \frac{1}{2}$ ;
- The Hilber-Hughes-Taylor  $\alpha$  (HHT- $\alpha$ ) method (see Refs. [3, 4]):

$$\alpha_m = 0, \quad \alpha = -\alpha_f \in \left[-\frac{1}{3}, 0\right], \quad \beta = \frac{(1 - \alpha)^2}{4}, \quad \gamma = \frac{1}{2} - \alpha.$$

The coefficients  $\alpha_m, \alpha_f, \beta, \gamma$  of the generalized- $\alpha$  method in Eq. (2-4) are usually chosen according to

$$\alpha_m = \frac{2\rho_\infty - 1}{1 + \rho_\infty}, \quad \alpha_f = \frac{\rho_\infty}{1 + \rho_\infty}, \quad \beta = \frac{(1 - \alpha)^2}{4}, \quad \gamma = \frac{1}{2} - \alpha,$$

where  $\alpha := \alpha_m - \alpha_f$  and  $\rho_\infty \in [0, 1]$  is a parameter controlling numerical dissipation ( $\rho_\infty = 0$  for maximal dissipation, see Ref. [2]).

In this paper we present extensions of the generalized- $\alpha$  method of Eqs. (2-4) for

- nonconstant mass matrix  $M(t, y)$ ;
- holonomic constraints  $g(t, y) = 0$ ;
- nonholonomic constraints  $k(t, y, y') = 0$ ;
- variable stepsizes  $h_n$ .

## 2 ABOUT THE NOTATION $a_\alpha, a_{1+\alpha}$

We use the notation  $a_\alpha$  and  $a_{1+\alpha}$  instead of  $a_0$  and  $a_1$  to emphasize the fact that these quantities should not be considered as approximations to the acceleration vector  $a(t)$  at  $t_0$  and  $t_1$  respectively, but at  $t_\alpha := t_0 + \alpha h$  and  $t_{1+\alpha} := t_1 + \alpha h = t_0 + (1 + \alpha)h$  respectively where  $\alpha := \alpha_m - \alpha_f$ . The reason is that for a solution  $(y(t), z(t), a(t))$  and values  $(y_0, z_0)$  satisfying  $y_0 - y(t_0) = O(h^2)$ ,  $z_0 - z(t_0) = O(h^2)$ , we have

$$a_{1+\alpha} - a(t_{1+\alpha}) = O(h^2) \quad \text{when} \quad a_\alpha - a(t_\alpha) = O(h^2), \quad (5)$$

whereas we only have  $a_{1+\alpha} - a(t_1) = O(h)$  when  $a_\alpha - a(t_0) = O(h^2)$  and  $\alpha \neq 0$ . This can be seen as follows. We rewrite Eq. (4) as

$$(1 - \alpha_m)a_{1+\alpha} + \alpha_m a_\alpha = (1 - \alpha_f)M^{-1}f(t_1, y_1, z_1) + \alpha_f M^{-1}f(t_0, y_0, z_0). \quad (6)$$

Since  $a(t) = M^{-1}f(t, y(t), z(t))$ ,  $y_1 - y(t_1) = O(h^2)$ , and  $z_1 - z(t_1) = O(h^2)$  we have

$$M^{-1}f(t_1, y_1, z_1) = a(t_0) + ha'(t_0) + O(h^2), \quad M^{-1}f(t_0, y_0, z_0) = a(t_0) + O(h^2).$$

Hence, for the right-hand side of Eq. (6) we obtain

$$(1 - \alpha_f)M^{-1}f(t_1, y_1, z_1) + \alpha_f M^{-1}f(t_0, y_0, z_0) = a(t_0) + h(1 - \alpha_f)a'(t_0) + O(h^2). \quad (7)$$

Since

$$a(t_{1+\alpha}) = a(t_0) + h(1 + \alpha)a'(t_0) + O(h^2), \quad a(t_\alpha) = a(t_0) + h\alpha a'(t_0) + O(h^2),$$

we have

$$(1 - \alpha_m)a(t_{1+\alpha}) + \alpha_m a(t_\alpha) = a(t_0) + h(1 - \alpha_m + \alpha)a'(t_0) + O(h^2). \quad (8)$$

Thus, from Eqs. (6-7-8), we obtain

$$(1 - \alpha_m)(a_{1+\alpha} - a(t_{1+\alpha})) + \alpha_m(a_\alpha - a(t_\alpha)) = h(-\alpha_f + \alpha_m - \alpha)a'(t_0) + O(h^2). \quad (9)$$

Hence, Eq. (5) is satisfied only for  $\alpha = \alpha_m - \alpha_f$ .

### 2.1 Defining $a_\alpha$ for the first step

The definition of  $a_\alpha$  for the first step remains. For  $\alpha_m = 0$ , for example for the HHT- $\alpha$  method, we see from Eq. (9) that taking  $a_\alpha = a_0$  where  $Ma_0 = f(t_0, y_0, z_0)$  still leads to the estimate  $a_{1+\alpha} - a(t_{1+\alpha}) = O(h^2)$ . When  $\alpha_m \neq 0$  it is better to define  $a_\alpha$  such that  $a_\alpha - a(t_\alpha) = O(h^2)$ , for example implicitly by

$$Ma_\alpha = (1 - \alpha)f(t_0, y_0, z_0) + \alpha f(t_1, y_1, z_1) \quad (10)$$

as proposed by Lunk and Simeon in Ref. [7]. Nevertheless, taking  $a_\alpha = a_0$  does not affect the order of global convergence of the  $y$  and  $z$  components, see Theorem 1 below.

### 3 NONCONSTANT MASS MATRIX $M(t, y)$

We consider  $M(t, y)y'' = f(t, y, y')$  where  $M(t, y)$  is a nonconstant mass matrix assumed to be invertible. These equations are equivalent to the semi-explicit system of index 1 DAEs

$$y' = z, \quad z' = a, \quad 0 = M(t, y)a - f(t, y, z).$$

A natural extension of the generalized- $\alpha$  method of Eqs. (2-4) is to replace Eq. (4) with

$$(1 - \alpha_m)M_{1+\alpha}a_{1+\alpha} + \alpha_m M_\alpha a_\alpha = (1 - \alpha_f)f(t_1, y_1, z_1) + \alpha_f f(t_0, y_0, z_0)$$

where

$$M_{1+\alpha} \approx M(t_{1+\alpha}, y(t_{1+\alpha})), \quad M_\alpha \approx M(t_\alpha, y(t_\alpha)).$$

For example we can take explicitly

$$M_{1+\alpha} := M(t_{1+\alpha}, y_0 + h(1 + \alpha)z_0), \quad M_\alpha := M_{(1+\alpha)-1} \text{ or } M(t_\alpha, y_0 + h\alpha z_0)$$

where  $M_{(1+\alpha)-1}$  denotes the matrix  $M_{1+\alpha}$  used at the previous time-step. Second order of convergence is a consequence of Theorem 1 below.

### 4 HOLONOMIC CONSTRAINTS $g(t, y) = 0$

We extend here the generalized- $\alpha$  method to systems in mechanics having holonomic constraints  $g(t, y) = 0$ . More precisely we consider

$$M(t, y)y'' = f(t, y, y', \lambda), \quad 0 = g(t, y),$$

where we usually have  $f(t, y, y', \lambda) = f_0(t, y, y') - g_y^T(t, y)\lambda$ . The term  $-g_y^T(t, y)\lambda$  represents reaction forces due to the holonomic constraints  $g(t, y) = 0$ . The algebraic variables  $\lambda$  are associated with the holonomic constraints. Differentiating  $0 = g(t, y)$  once with respect to  $t$  we obtain

$$0 = (g(t, y))' = g_t(t, y) + g_y(t, y)y'.$$

Thus we consider systems of index 2 overdetermined differential-algebraic equations (ODAEs) of the form

$$y' = z, \quad z' = a, \quad 0 = M(t, y)a - f(t, y, z, \lambda), \quad 0 = g(t, y), \quad 0 = g_t(t, y) + g_y(t, y)z,$$

and we assume the matrix

$$\begin{bmatrix} M(t, y) & -f_\lambda(t, y, z, \lambda) \\ g_y(t, y) & O \end{bmatrix} \text{ is invertible.}$$

For  $f(t, y, z, \lambda) = f_0(t, y, z) - g_y^T(t, y)\lambda$ , this matrix becomes

$$\begin{bmatrix} M(t, y) & g_y^T(t, y) \\ g_y(t, y) & O \end{bmatrix}$$

and is symmetric when  $M(t, y)$  is symmetric. At  $t_0$  we consider consistent initial conditions  $(y_0, z_0, a_0, \lambda_0)$ , i.e.,

$$\begin{aligned} 0 &= M(t_0, y_0)a_0 - f(t_0, y_0, z_0, \lambda_0), \\ 0 &= g(t_0, y_0), \\ 0 &= g_t(t_0, y_0) + g_y(t_0, y_0)z_0, \\ 0 &= g_{tt}(t_0, y_0) + 2g_{ty}(t_0, y_0)z_0 + g_{yy}(t_0, y_0)(z_0, z_0) + g_y(t_0, y_0)a_0. \end{aligned}$$

Several extensions of the HHT- $\alpha$  method have been proposed. Cardona and Géradin in Ref. [1] analyze a direct extension of the HHT- $\alpha$  method to linear DAEs where it was shown that a direct application of the HHT- $\alpha$  method is inconsistent and suffers from instabilities. Yen, Petzold, and Raha in Ref. [8] propose a first order extension of the HHT- $\alpha$  method based on projecting the solution of the underlying ODEs onto the constraints (including the index 1 acceleration level constraints) after each step. More recently, second order extensions of the HHT- $\alpha$  method and generalized- $\alpha$  method have been proposed independently by Jay and Negrut in Ref. [5] and by Lunk and Simeon in Ref. [7] based on the additivity of  $f(t, y, z, \lambda) = f_0(t, y, z) + f_1(t, y, \lambda)$ . Here, we propose a different and more natural extension of the generalized- $\alpha$  method which does not use this additive structure

$$\begin{aligned}
 y_1 &= y_0 + h z_0 + \frac{h^2}{2} ((1 - 2\beta)a_\alpha + 2\beta\tilde{a}_{1+\alpha}), \\
 z_1 &= z_0 + h ((1 - \gamma)a_\alpha + \gamma a_{1+\alpha}), \\
 (1 - \alpha_m)M_{1+\alpha}\tilde{a}_{1+\alpha} + \alpha_m M_\alpha a_\alpha &= (1 - \alpha_f)f(t_1, y_1, z_1, \tilde{\lambda}_1) + \alpha_f f(t_0, y_0, z_0, \lambda_0), \quad (11) \\
 (1 - \alpha_m)M_{1+\alpha}a_{1+\alpha} + \alpha_m M_\alpha a_\alpha &= (1 - \alpha_f)f(t_1, y_1, z_1, \lambda_1) + \alpha_f f(t_0, y_0, z_0, \lambda_0), \\
 0 &= g(t_1, y_1), \\
 0 &= g_t(t_1, y_1) + g_y(t_1, y_1)z_1.
 \end{aligned}$$

For  $f(t, y, z, \lambda) = f_0(t, y, z) - g_y^T(t, y)\lambda$  we can replace for example Eq. (11) by

$$(1 - \alpha_m)M_{1+\alpha}(a_{1+\alpha} - \tilde{a}_{1+\alpha}) = (1 - \alpha_f)g_y^T(t_1, y_1)(\tilde{\lambda}_1 - \lambda_1).$$

Second order of convergence is a consequence of Theorem 1 below.

## 5 NONHOLONOMIC CONSTRAINTS $k(t, y, y') = 0$

We extend here the generalized- $\alpha$  method to systems in mechanics having nonholonomic constraints  $k(t, y, y') = 0$ . More precisely we consider

$$M(t, y)y'' = f(t, y, y', \psi), \quad 0 = k(t, y, y')$$

where we usually have  $f(t, y, y', \psi) = f_0(t, y, y') - k_{y'}^T(t, y, y')\psi$ . The term  $-k_{y'}^T(t, y, y')\psi$  represents reaction forces due to the nonholonomic constraints  $k(t, y, y') = 0$ . The algebraic variables  $\psi$  are associated respectively with the nonholonomic constraints. Hence, we consider systems of index 2 differential-algebraic equations (DAEs) of the form

$$y' = z, \quad z' = a, \quad 0 = M(t, y)a - f(t, y, z, \psi), \quad 0 = k(t, y, z),$$

and we assume the matrix

$$\begin{bmatrix} M(t, y) & -f_\psi(t, y, z, \psi) \\ k_z(t, y, z) & O \end{bmatrix} \text{ is invertible .}$$

For  $f(t, y, z, \psi) = f_0(t, y, z) - k_z^T(t, y, z)\psi$ , this matrix becomes

$$\begin{bmatrix} M(t, y) & k_z^T(t, y, z) \\ k_z(t, y, z) & O \end{bmatrix}$$

and is symmetric when  $M(t, y)$  is symmetric. At  $t_0$  we consider consistent initial conditions  $(y_0, z_0, a_0, \psi_0)$ , i.e.,

$$\begin{aligned} 0 &= M(t_0, y_0)a_0 - f(t_0, y_0, z_0, \psi_0), \\ 0 &= k(t_0, y_0, z_0), \\ 0 &= k_t(t_0, y_0, z_0) + k_y(t_0, y_0, z_0)z_0 + k_z(t_0, y_0, z_0)a_0. \end{aligned}$$

We propose the following extension of the generalized- $\alpha$  method:

$$\begin{aligned} y_1 &= y_0 + h z_0 + \frac{h^2}{2} ((1 - 2\beta)a_\alpha + 2\beta a_{1+\alpha}), \\ z_1 &= z_0 + h ((1 - \gamma)a_\alpha + \gamma a_{1+\alpha}), \\ (1 - \alpha_m)M_{1+\alpha}a_{1+\alpha} + \alpha_m M_\alpha a_\alpha &= (1 - \alpha_f)f(t_1, y_1, z_1, \psi_1) + \alpha_f f(t_0, y_0, z_0, \psi_0), \\ 0 &= k(t_1, y_1, z_1). \end{aligned}$$

Second order of convergence is a consequence of Theorem 1 below.

## 6 GENERAL EXTENSION AND CONVERGENCE

We extend the generalized- $\alpha$  method to systems in mechanics having a nonconstant mass matrix  $M(t, y)$ , holonomic constraints  $g(t, y) = 0$ , and nonholonomic constraints  $k(t, y, y') = 0$ . The algebraic variables  $\lambda$  are associated with the holonomic constraints  $g(t, y) = 0$  and  $g_t(t, y) + g_y(t, y)y' = 0$  which result from differentiating  $g(t, y) = 0$  with respect to  $t$ . The algebraic variables  $\psi$  are associated with the nonholonomic constraints  $k(t, y, y') = 0$ . Thus we consider systems of index 2 overdetermined differential-algebraic equations (ODAEs) of the form

$$\begin{aligned} y' &= z, \\ M(t, y)z' &= f(t, y, z, \lambda, \psi), \\ 0 &= g(t, y), \\ 0 &= g_t(t, y) + g_y(t, y)z, \\ 0 &= k(t, y, z), \end{aligned} \tag{12}$$

and we assume the matrix

$$\begin{bmatrix} M(t, y) & -f_\lambda(t, y, z, \lambda, \psi) & -f_\psi(t, y, z, \lambda, \psi) \\ g_y(t, y) & O & O \\ k_z(t, y, z) & O & O \end{bmatrix} \text{ is invertible.} \tag{13}$$

For  $f(t, y, z, \lambda, \psi) = f_0(t, y, z) - g_y^T(t, y)\lambda - k_z^T(t, y, z)\psi$ , this matrix becomes

$$\begin{bmatrix} M(t, y) & g_y^T(t, y) & k_z^T(t, y, z) \\ g_y(t, y) & O & O \\ k_z(t, y, z) & O & O \end{bmatrix}$$

and is symmetric when  $M(t, y)$  is symmetric. At  $t_0$  we consider consistent initial conditions  $(y_0, z_0, a_0, \lambda_0, \psi_0)$ , i.e.,

$$0 = M(t_0, y_0)a_0 - f(t_0, y_0, z_0, \lambda_0, \psi_0),$$

$$\begin{aligned}
 0 &= g(t_0, y_0), \\
 0 &= g_t(t_0, y_0) + g_y(t_0, y_0)z_0, \quad 0 = k(t_0, y_0, z_0), \\
 0 &= g_{tt}(t_0, y_0) + 2g_{ty}(t_0, y_0)z_0 + g_{yy}(t_0, y_0)(z_0, z_0) + g_y(t_0, y_0)a_0, \\
 0 &= k_t(t_0, y_0, z_0) + k_y(t_0, y_0, z_0)z_0 + k_z(t_0, y_0, z_0)a_0.
 \end{aligned}$$

Here, we propose an extension of the generalized- $\alpha$  method which does not use any additive structure of  $f(t, y, z, \lambda, \psi)$ . We call it the *generalized- $\alpha$ -SOI2 method* (SOI2 stands for Stabilized Overdetermined Index 2). One step  $(t_0, y_0, z_0, a_\alpha, \lambda_0, \psi_0) \mapsto (t_1, y_1, z_1, a_{1+\alpha}, \lambda_1, \psi_1)$  with stepsize  $h$  of the generalized- $\alpha$ -SOI2 method for Eq. (12) can be expressed as follows

$$\begin{aligned}
 y_1 &= y_0 + h z_0 + \frac{h^2}{2} ((1 - 2\beta)a_\alpha + 2\beta\tilde{a}_{1+\alpha}), \\
 \tilde{z}_1 &= z_0 + h ((1 - \gamma)a_\alpha + \gamma\tilde{a}_{1+\alpha}), \\
 z_1 &= z_0 + h ((1 - \gamma)a_\alpha + \gamma a_{1+\alpha}), \\
 (1 - \alpha_m)M_{1+\alpha}\tilde{a}_{1+\alpha} + \alpha_m M_\alpha a_\alpha &= (1 - \alpha_f)f(t_1, y_1, z_1, \tilde{\lambda}_1, \tilde{\psi}_1) + \alpha_f f(t_0, y_0, z_0, \lambda_0, \psi_0), \\
 (1 - \alpha_m)M_{1+\alpha}a_{1+\alpha} + \alpha_m M_\alpha a_\alpha &= (1 - \alpha_f)f(t_1, y_1, z_1, \lambda_1, \psi_1) + \alpha_f f(t_0, y_0, z_0, \lambda_0, \psi_0), \\
 0 &= g(t_1, y_1), \\
 0 &= g_t(t_1, y_1) + g_y(t_1, y_1)z_1, \\
 0 &= k(t_1, y_1, \tilde{z}_1), \\
 0 &= k(t_1, y_1, z_1),
 \end{aligned} \tag{14}$$

where  $M_{1+\alpha} := M(t_{1+\alpha}, y_0 + h(1 + \alpha)z_0)$  and  $M_\alpha := M_{(1+\alpha)-1}$  or  $M(t_\alpha, y_0 + h\alpha z_0)$ . The auxiliary variables  $\tilde{z}_1, \tilde{a}_{1+\alpha}, \tilde{\lambda}_1, \tilde{\psi}_1$  are just local to the current step, they are not propagated. For  $f(t, y, z, \lambda, \psi) = f_0(t, y, z) - g_y^T(t, y)\lambda - k_z^T(t, y, z)\psi$  we can replace for example

$$(1 - \alpha_m)M_{1+\alpha}\tilde{a}_{1+\alpha} + \alpha_m M_\alpha a_\alpha = (1 - \alpha_f)f(t_1, y_1, z_1, \tilde{\lambda}_1, \tilde{\psi}_1) + \alpha_f f(t_0, y_0, z_0, \lambda_0, \psi_0)$$

by

$$(1 - \alpha_m)M_{1+\alpha}(a_{1+\alpha} - \tilde{a}_{1+\alpha}) = (1 - \alpha_f)g_y^T(t_1, y_1)(\tilde{\lambda}_1 - \lambda_1) + (1 - \alpha_f)k_z^T(t_1, y_1, z_1)(\tilde{\psi}_1 - \psi_1).$$

From Ref. [6] we have the following convergence result:

**Theorem 1.** *Consider the overdetermined system of DAEs given by Eq. (12) and assumption Eq. (13) with consistent initial conditions  $(y_0, z_0, a_0, \lambda_0, \psi_0)$  at  $t_0$  and exact solution  $(y(t), z(t), a(t), \lambda(t), \psi(t))$ . Suppose that  $a_\alpha - a(t_0 + \alpha h) = O(h)$ , for example  $a_\alpha := a_0$ . Then the generalized- $\alpha$ -SOI2 numerical approximation  $(y_n, z_n, a_{n+\alpha}, \lambda_n, \psi_n)$  (see Eq. (14)) satisfies for  $0 \leq h \leq h_{\max}$  and  $t_n - t_0 = nh \leq \text{Const}$*

$$\begin{aligned}
 y_n - y(t_n) &= O(h^2), \quad z_n - z(t_n) = O(h^2), \quad a_{n+\alpha} - a(t_n + \alpha h) = O(h^2 + r^n h), \\
 \lambda_n - \lambda(t_n) &= O(h^2 + r^n h), \quad \psi_n - \psi(t_n) = O(h^2 + r^n h)
 \end{aligned}$$

where  $r := |\alpha_m / (1 - \alpha_m)|$ . Moreover, if  $\alpha_m = 0$  or  $a_\alpha - a(t_0 + \alpha h) = O(h^2)$  then we have

$$a_{n+\alpha} - a(t_n + \alpha h) = O(h^2), \quad \lambda_n - \lambda(t_n) = O(h^2), \quad \psi_n - \psi(t_n) = O(h^2).$$

## 7 VARIABLE STEPSIZES $h_n$

When applying the generalized- $\alpha$  method with variable stepsizes, the values  $a_{n+\alpha}$  and  $M_{n+\alpha}a_{n+\alpha}$  must be adjusted before each new step in order to preserve the second order of the method. Consider a previous step starting at  $t_{n-1}$  with stepsize  $h_{n-1}$  and a new step starting at  $t_n = t_{n-1} + h_{n-1}$  with stepsize  $h_n$ . The value  $a_{n-1+\alpha}$  used in the previous step is an approximation of  $a(t)$  at  $t_{n-1} + \alpha h_{n-1}$  i.e.,  $a_{n-1+\alpha} \approx a(t_{n-1} + \alpha h_{n-1})$ . The value  $a_{n+\alpha}$  obtained in the previous step is an approximation of  $a(t)$  at  $t_{n-1} + (1 + \alpha)h_{n-1} = t_n + \alpha h_{n-1}$  i.e.,  $a_{n+\alpha} \approx a(t_n + \alpha h_{n-1})$ . For the current timestep starting at  $t_n$  with stepsize  $h_n$  we need the value  $a_{n+\alpha}$  to be an approximation of  $a(t)$  at  $t_n + \alpha h_n$ , i.e.,  $a_{n+\alpha} \approx a(t_n + \alpha h_n)$ . By linearly interpolating  $a_{n-1+\alpha}$  at  $t_{n-1} + \alpha h_{n-1}$  and  $a_{n+\alpha}$  at  $t_n + \alpha h_{n-1}$  and by extrapolating at  $t_n + \alpha h_n$ ,  $a_{n+\alpha}$  can be replaced by

$$a_{n+\alpha} \leftarrow a_{n+\alpha} + \alpha \left( \frac{h_n}{h_{n-1}} - 1 \right) (a_{n+\alpha} - a_{n-1+\alpha}). \quad (15)$$

A similar formula for  $M_{n+\alpha}a_{n+\alpha}$  should also be used. We can replace  $M_{n+\alpha}a_{n+\alpha}$  by

$$M_{n+\alpha}a_{n+\alpha} \leftarrow M_{n+\alpha}a_{n+\alpha} + \alpha \left( \frac{h_n}{h_{n-1}} - 1 \right) (M_{n+\alpha}a_{n+\alpha} - M_{n-1+\alpha}a_{n-1+\alpha}). \quad (16)$$

These formulas have several advantages:

- they are simple to implement;
- their computational cost is almost negligible;
- they are valid for both ODEs and DAEs;
- they preserve second order of convergence.

These modifications are not necessary to preserve the second order of convergence for the  $y$  and  $z$  variables. However, since the cost of these modifications is negligible and they also allow second order of convergence for the  $a$ ,  $\lambda$ , and  $\psi$  variables, these modifications are recommended.

## 8 NUMERICAL EXAMPLE

To illustrate Theorem 1 numerically we consider the following mathematical test problem

$$\begin{aligned} y_1' &= z_1, & y_2' &= z_2, \\ \begin{bmatrix} y_1 & y_2 - e^{-2t} \\ \sin(y_1 - e^t) & y_1 y_2 \end{bmatrix} \begin{bmatrix} z_1' \\ z_2' \end{bmatrix} &= \begin{bmatrix} e^t(y_1 z_2 + 2y_2 z_1) + e^{2t}y_1 \lambda_1 - y_1 z_2 \psi_1 - 2 \\ e^{-t}(y_2 z_2/2 - 2y_1 z_1 y_2 z_2 + y_2 \lambda_1^2) - y_1 y_2 z_1 \psi_1^3 + e^{3t} \end{bmatrix}, \\ 0 &= g(t, y) = y_1^2 y_2 - 1, \\ 0 &= g_t(t, y) + g_y(t, y)z = 2y_1 y_2 z_1 + y_1^2 z_2, \\ 0 &= k(t, y, z) = y_1 z_1 z_2 + 2. \end{aligned}$$

We have applied the generalized- $\alpha$ -SOI2 method (see Eq. (14)) with damping parameter  $\rho_\infty = 0.2$  and variable stepsizes alternating between  $h/3$  and  $2h/3$  for various values of  $h$ . Using the modification of  $a_{n+\alpha}$  of Eq. (15) and  $M_{n+\alpha}a_{n+\alpha}$  of Eq. (16) we observe global convergence of order 2 at  $t_n = 1$  in Fig. 1. Without these modifications in Fig. 2 we observe a reduction of the order of convergence to 1 for the variables  $a$ ,  $\lambda$ ,  $\psi$ .



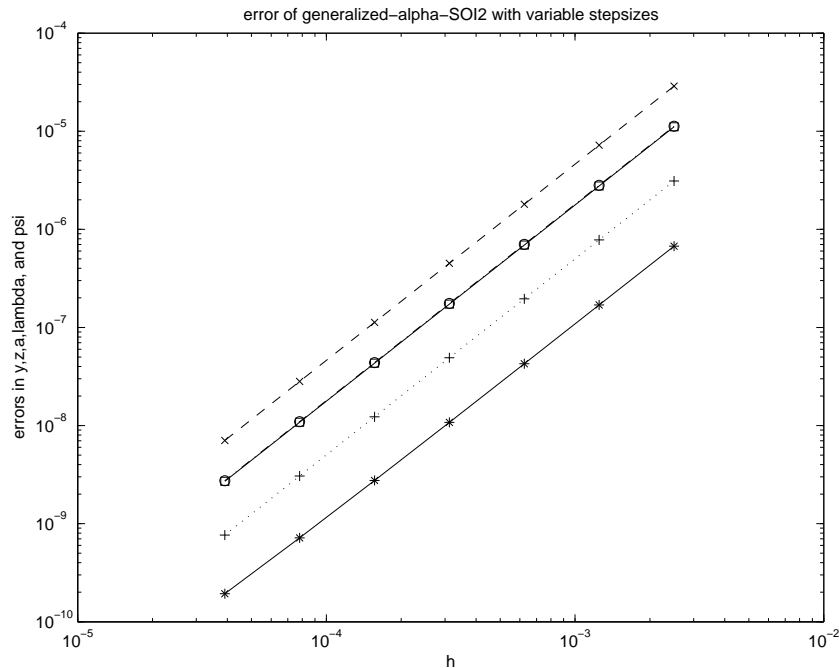


Figure 1: Global errors  $\|y_n - y(t_n)\|_2$  ( $\square$ ),  $\|z_n - z(t_n)\|_2$  ( $\circ$ ),  $\|a_{n+\alpha} - a(t_n + \alpha h)\|_2$  ( $\times$ ),  $\|\lambda_n - \lambda(t_n)\|_2$  ( $+$ ),  $\|\psi_n - \psi(t_n)\|_2$  ( $*$ ) of the generalized- $\alpha$ -SOI2 method ( $\rho_\infty = 0.2$ ) at  $t_n = 1$  for a test problem with variable stepsizes alternating between  $h/3$  and  $2h/3$  with modification of  $a_{n+\alpha}$  of Eq. (15) and  $M_{n+\alpha}a_{n+\alpha}$  of Eq. (16).

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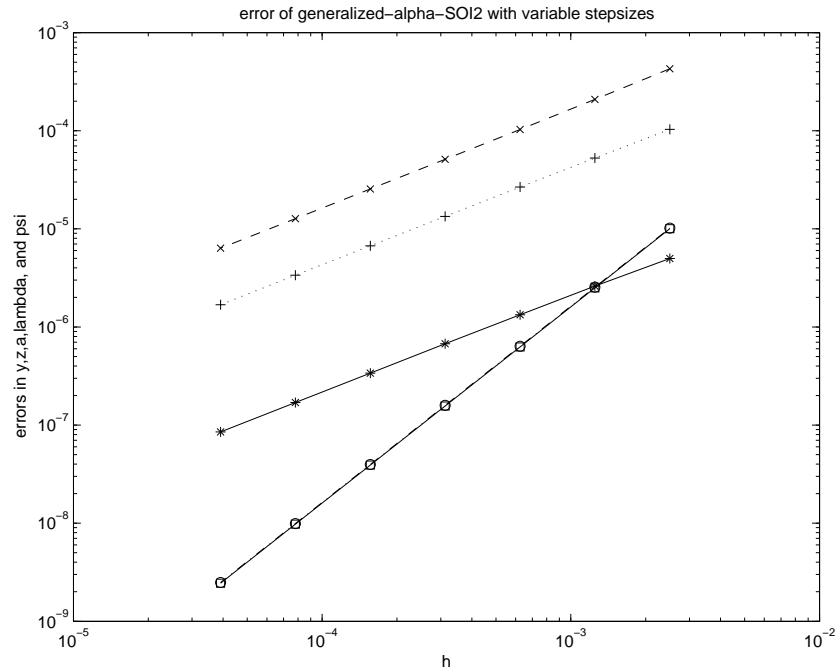


Figure 2: Global errors  $\|y_n - y(t_n)\|_2$  ( $\square$ ),  $\|z_n - z(t_n)\|_2$  ( $\circ$ ),  $\|a_{n+\alpha} - a(t_n + \alpha h)\|_2$  ( $\times$ ),  $\|\lambda_n - \lambda(t_n)\|_2$  ( $+$ ),  $\|\psi_n - \psi(t_n)\|_2$  ( $*$ ) of the generalized- $\alpha$ -SOI2 method ( $\rho_\infty = 0.2$ ) at  $t_n = 1$  for a test problem with variable stepsizes alternating between  $h/3$  and  $2h/3$  without modification of  $a_{n+\alpha}$  of Eq. (15) and  $M_{n+\alpha}a_{n+\alpha}$  of Eq. (16).